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PATENT APPLICATION OF

JING GUI, BRUNO JEAN MARCHON,  
HUAN TANG, AND  
ZINE-EDDINA BOUTAGHOU

ENTITLED

PRESSURE RELIEF TRENCHES FOR SLIP HEADS TO  
REDUCE STICTION

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**SLIDER WITH PRESSURE RELIEF TRENCHES**  
**CROSS-REFERENCE TO RELATED APPLICATION**

This application claims priority to  
Provisional Application Serial No. 60/088,119, filed  
5 June 4, 1998, and entitled "PRESSURE-RELIEF TRENCHES FOR  
SLIP HEADS TO REDUCE STICTION."

**BACKGROUND OF THE INVENTION**

The present invention relates to a data  
storage system. In particular, the present invention  
10 relates to a slider with improved meniscus stiction  
control.

Disc drives are well known in the industry.  
Such drives use rigid discs coated with a magnetizable  
medium for storage of digital information in a plurality  
15 of concentric data tracks. Typically, disc drives  
include a disc pack including a plurality of concentric  
discs mounted on a spindle motor which causes the discs  
to spin. Heads carrying transducer elements are  
supported relative to the disc surfaces to read and or  
20 write digital information to the disc surfaces.

Heads include a slider supported via a  
suspension assembly coupled to an actuator or "E" block.  
Sliders include an air bearing surface which faces the  
disc surface. As the disc rotates, the disc drags air  
25 onto the slider along the air bearing surface in a  
direction approximately parallel to the tangential  
velocity of the disc. As the air passes beneath the air  
bearing surface, the pressure between the disc and the  
air bearing surface increases, which creates a  
30 hydrodynamic lifting force that causes the slider to  
lift directly above the disc surface to read and/or  
write data to the surface of the disc.

Prior to rotation of the disc, the slider  
rests on the disc surface. The slider is not lifted

from the disc until the hydrodynamic lifting force, caused by rotation of the disc, is sufficient to overcome a preload force supplied to bias the slider toward the disc surface, and a stiction force holding the slider to the disc surface. The hydrodynamic properties of the slider are affected by the speed of rotation of the disc, the design of the air bearing surface of the slider, and the preload force supplied to the slider via the suspension assembly.

Typically a lubricant coating covers the disc surface to protect the slider and disc from wear during contact starts and stops (CSS). Contact between the slider and disc surface (and lubricant coating) creates a meniscus effect which increases stiction force between the slider and disc surface. When a disc drive is turned on, the spindle motor produces torque to overcome stiction and initiate "spin-up". Stiction increases the motor torque required to spin-up the disc drive. If stiction is too large for motor torque to overcome, spin-up failure could occur.

Prior disc drives include both landing zones and data zones on the disc surface. The slider rests on the landing zone for CSS. The landing zone is textured to provide a roughened surface structure for reducing stiction between the slider and disc surface for take-off. However, the textured surface of the landing zone limits the fly-height of the slider. The present invention relates to these and other problems.

#### SUMMARY OF THE INVENTION

The present invention relates to a slider for supporting transducer elements for a data storage system including at least one pressure relief trench formed in the raised bearing surface proximate to a contact

interface position between the slider and disc surface. The trench is sized to reduce capillary pressure of the meniscus relative to the disjoining pressure of a lubricant film layer on the disc surface to limit the area or expansion of a film bridge or meniscus between the bearing surface of the slider and disc surface.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a perspective view of an embodiment of a data storage system.

FIG. 2 is a perspective view of an embodiment of an actuator block supporting disc heads.

FIG. 3 is a perspective view of an embodiment of a slider supporting transducers.

FIG. 4 is a side illustrative view of the slider of FIG. 3 supported on a lubricant film layer on the disc surface.

FIG. 5 is a side illustrative view of a trailing edge portion of a slider tipped toward the disc surface.

FIG. 6 is a graphical illustration of stiction force of two sample sliders subjected to a forward and a reverse or backward rotation.

FIGS. 7-1 - 7-4 are illustrative views of various wetting regimes of a slider-disc interface.

FIG. 8 graphically illustrates different slider - disc interface regimes.

FIG. 9 is a perspective illustration of an embodiment of a slider according to the present invention.

FIG. 10 is a detailed perspective illustration of a center rail portion of the slider of FIG. 9 including a trench.

FIG. 11 is an illustrative view of a slider disc interface for cross-sectional portion 11--11 of FIG. 9.

5 FIG. 12 is a perspective illustration of an alternate embodiment trench pattern on a slider of the present invention.

FIG. 13 is a detailed perspective illustration of an alternate embodiment trench pattern of the present invention.

10 FIG. 14 is a detailed perspective illustration of an alternate embodiment trench pattern of the present invention.

FIG. 15 is a detailed perspective illustration of an alternate embodiment trench pattern of the present invention.

15 FIG. 16 is a detailed perspective illustration of an alternate embodiment trench pattern of the present invention.

FIG. 17 is a perspective view of an embodiment of a slider for pseudo-contact recording.

#### DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

FIG. 1. illustrates a disc drive 50 including a chassis 52, discs 54, and actuator assembly 56. Discs 25 54 are rotationally coupled to chassis 52 via a spindle motor (not shown) for rotation, as illustrated by arrow 58. Actuator assembly 56 rotationally supports heads 60 for reading and/or writing data to and from discs 54. The actuator assembly includes actuator block 62 and voice coil motor (VCM) 64. As shown, actuator block 62 30 is rotationally coupled to chassis 52. The actuator block 62 includes a plurality of actuator arms 66 (only one shown in FIG. 1) to support heads 60 relative to the disc surface. The actuator block rotates as illustrated

by arrow 68 to move heads 60 along an arcuate path for placement relative to data tracks of a disc 54 to read or write data relative to the disc surface. Movement of the actuator block 62 is controlled by voice coil motor 5 64, which is coupled to control circuitry of the disc drive illustrated by block 70.

As shown in FIG. 2, heads 60 include a slider 72 which supports transducer elements for read and write operations. Slider 72 is coupled to actuator block 62 10 via a suspension assembly 74 coupled to actuator arms 66. As shown in FIG. 2, suspension assembly 74 includes a load beam 76 and a gimbal spring 78. Gimbal spring 78 supports slider 72 to pitch, roll and follow the topography of the disc in a known manner. FIG. 3 15 illustrates one embodiment of a slider 72 formed of a rigid member including a leading edge 80, a trailing edge 82, an upper surface 84, and a lower air bearing surface 86. The upper surface 84 is operably coupled to gimbal spring 78 shown in FIG. 2 to flexibly support 20 slider 72. Load beam 76 supplies a preload force to bias the slider 72 toward the disc surface 54.

The lower air bearing surface 86 of the slider 72 faces the disc surface and includes raised side rails 90 and 92, and a center rail 94. Slider 72 includes a 25 sloped leading surface 96 for "take-off". Center rail supports transducer 98 (illustrated diagrammatically) for read or write operations. Transducers may be inductive type transducers or magnetoresistive transducers. Discs 54 are rotated to create a 30 hydrodynamic lifting force to lift the head 60 (slider 72) above the disc surface for proximity recording. Although a particular bearing surface is shown, it should be understood that alternate bearing designs may

be used and application is not limited to a particular bearing design.

Prior to operation, the slider 72 is parked on the disc surface for contact starts and stops ("CSS").

5 The disc surface 54 includes a lubricant coating to limit wear of the slider and disc during CSS. Interface between the slider and lubricant creates a meniscus effect which increases the stiction between the slider and disc surface. Increase in stiction in the presence

10 of a liquid lubricant is a direct result of the meniscus effect of the lubricant. The influence of the meniscus is related to the thickness of the lubricant coating and contact interface and separation between the slider and disc surface. Prior discs have separate textured

15 landing zones to park the slider prior to operation to limit stiction between the slider and disc surface.

In the present application, the slider includes pads 100a- 100b or SLIP (Slider Landing Integrated Pad) extending from the bearing surface to

20 support the slider above the disc surface for contact starts and stops as illustrated in FIG. 3-4. In the embodiment illustrated, landing pads 100a, 100b extend from, or are elevated above the bearing surface 86 proximate to the leading and trailing ends 80, 82,

25 respectively to support the slider 72 above the disc surface 54 for CSS.

In operation, rotation of the discs 54 creates a fluid or air flow under the bearing surface from the leading edge surface 96 to raise the slider 72 above the

30 disc surface for proximity recording. Sufficient lift must be imparted to the bearing surface 86 to overcome the stiction holding the slider 72 to the disc surface and the preload force supplied by the suspension assembly 74. As previously explained, for operation or

"take-off", the motor torque of the spindle motor must overcome the stiction force holding the slider to the disc surface. Stiction force  $F_s$  is proportional to the preload force  $F_1$  and the meniscus force  $F_m$  as follows:

5

$$F_s = \mu(F_m + F_1) \quad \text{Eq. 1}$$

where:

10  $F_m$  - is the meniscus force created by the interface of the lubricant film and the slider; and

$F_1$  - is the pre-load force supplied to the slider by the suspension assembly to bias the slider toward the disc surface.

15

Pads are adapted to support slider 72 above a relatively smooth disc surface coated with a lubricant film layer 102 as illustrated in FIG. 4 to reduce stiction between the slider and disc surface for CSS.

20 Sliders typically fly above the disc surface at a pitch angle so that the trailing edge 82 supporting the transducer elements flies closer to the disc surface than the leading edge 80. Areal disc drive density is increasing and slider fly height is decreasing for desired read or write resolution. As shown in FIG. 4, 25 pads 100b are recessed a distance 104 from the transducer 98 and trailing edge to limit contact interference between the pad 100b and the disc surface. The recessed position of pad 100b (or absence of pad 100b at the trailing edge 82) increases the propensity 30 of the slider to tip so that trailing edge contacts or touches the lubricant film 102 on the disc surface as illustrated in FIG. 5.

In particular, as shown, a trailing edge portion of the slider 72 spaced from pad 100b (not

shown) tips toward the disc surface to contact the lubricant film layer 102. Interface between the slider surface and lubricant film layer 102 creates meniscus 106 between the lubricant film layer 102 and slider 72. Interaction between the slider 72 and the lubricant film layer 102 is confirmed experimentally in FIG. 6. FIG. 6 shows the experimental results of two test sliders 110, 112 each subjected to a manual rotation in the forward direction (from the leading edge to the trailing edge) and backward direction (from the trailing edge to the leading edge prior to stiction measurement. The sliders 110, 112 include recessed pads 100b having a recessed dimension 104 of 13 mils. The sliders 110, 112 were tested on two smooth discs having a Ra (Roughness Average) of 7 Angstroms and a lubricant film layer thickness 102 of 30 Angstroms.

The stiction force 114 of the slider 110, 112 relative to the disc surface was measured for each rotation direction. As shown, the stiction 114-1 for slider 110 in the forward rotation direction was significantly less than the stiction 114-2 measured in the backward rotation direction. Similarly, the stiction force 114-3 for slider 112 in the forward direction was significantly less than the stiction force 114-4 measured in the backward rotation direction. The large discrepancy in stiction is attributed to an increase meniscus 106 introduced by the slider tipping as illustrated in FIG. 5 when the slider was subjected to a backward rotation direction of the disc prior to stiction measurement so that the friction force drives the slider towards tipping.

To form the menisci, the lubricant is dragged from the contact area between the slider and disc surface along the surface of the slider (herein

capillary surface), via capillary pressure. The lubricant film is dragged so that the effect of the meniscus expands, while the attractive force between lubricant molecules and the solid surface, which is  
5 quantitatively represented by the disjoining pressure of the lubricant film, is overcome by the driving force of the capillary pressure of the meniscus. The magnitude of meniscus force  $F_m$  and stiction for the slider is proportional to the area of the meniscus. In particular  
10 stiction force  $F_s$  (in grams-force gf) may be estimated as follows:

$$F_s \approx 0.0005A$$

where:

A is the area of the meniscus in  $\mu\text{m}^2$ .

15 For example, every  $2,000 \mu\text{m}^2$  of meniscus creates 1gf of stiction. Thus, in the embodiment of the slider 72 illustrated in FIGS. 3-4, the center rail 94 is approximately  $70,000 \mu\text{m}^2$  and thus if half the center rail is flooded an estimated stiction force is  
20 approximately 17.5 gf. The increase in stiction force as illustrated above affects operation of the disc drive.

As the lubricant film is thinned, it is more and more difficult for a meniscus to draw lubricant from its surrounding area to spread. Eventually, a (quasi)  
25 equilibrium state is reached where the disjoining pressure of the film equals the capillary pressure of the meniscus as follows:

$$\frac{A_H}{6\pi d^3} = \frac{\gamma}{R_e}$$

where:

30  $A_H$  is the Hamaker constant

$\gamma$  - is surface tension of the lubricant;

$R_e$  - is the radius of the leading edge 115 of the meniscus formed between the disc and capillary surface of the slider.

$d$  - is the thickness of the lubricant film.

5        The Hamaker constant  $A_H$  is  $\sim 10^{-19}$  Joules for most PFPE lubricants on carbon. The surface tension for Zdol and most other PFPE lubricants is approximately  $\sim 25 \text{ mN/m}$ . For the tipped slider illustrated in FIG. 5, the equilibrium condition is related to the thickness  $d$  of the lubricant film layer 102 and the geometry or  
10        interface between the tipped slider 72 and disc surface. In the embodiment illustrated in FIG. 5, the separation distance  $h$  increases from the trailing edge contact position along the length of the slider 72. The radius  
15        of the meniscus 106 is the separation distance  $h/2$  between the slider 72 and disc surface at the leading edge 115 of the meniscus 106.

FIG. 7-1 - FIG. 7-4 illustrate different wetting regimes for a head-disc contact interface with respect to bumps 116. FIG. 7-1 is referred to as a toe-dipping regime. FIG. 7-2 is referred to as a pillbox regime. FIG. 7-3 is referred to as a flooded regime and FIG. 7-4 is referred to as the immersed regime. The toe-dipping regime provides the least stiction and the  
20        flooded regime introduces the highest stiction since the surface area interface of the meniscus and the slider increases from the toe-dipping regime to the immersed regime. Thus, it is desirable to provide a contact interface between the disc and slider in the toe-dipping  
25        regime to control stiction.  
30       

In particular, in the toe-dipping regime, illustrated in FIG. 7-1, bumps 116 contact lubricant film 102 developing a meniscus 106 at the interface between the bump 116 and lubricant film 102. The

meniscus 106 expands until radius  $R_e$  of the meniscus is at equilibrium as defined by Eq. 1.  $2R_e$  at equilibrium is less than the separation distance 120 between the slider and the disc so that the meniscus area does not extend or spread between the slider 72 and the disc surface. In the pillbox regime illustrated in FIG. 7-2,  $2R_e$  at equilibrium for lubricant thickness  $d$  is similar to the separation distance 120 of the head - disc. FIGS. 7-3 and 7-4 illustrate equilibrium positions where the meniscus film envelopes the separation between the disc and slider so that the slider is essentially glued to the disc surface by the lubricant film.

FIG. 8 illustrates a graphical relation between the head - disc separation 120, lubricant thickness and meniscus equilibrium condition. Line 122 illustrates separation of the toe-dipping regime 124 and pillbox and flooded regimes 126 based upon lubricant thickness  $d$  and slider - disc separation 120. The meniscus expands depending upon the lubricant thickness and separation distance  $h$  (120) to an equilibrium in the toe-dipping regime 124 or pillbox or flooded regimes 126. As shown, for a greater lubricant thickness  $d$ , the greater the slider - disc separation 120 require to limit meniscus effect to the toe-dipping regime 124. To reduce meniscus size, lubricant thickness  $d$  may be decreased or slider disc separation 120 may be increased. However, operating requirements may limit parameter adjustments to control meniscus growth.

The present invention provides a slider-disc interface to limit influence of the meniscus effect as illustrated in an embodiment of the invention shown in FIGS. 9-11. As shown in FIGS. 9-11, slider includes a longitudinal axis parallel to side 127, 128 of slider and a transverse axis generally perpendicular to the

longitudinal axis. Slider 72 includes an elongated trench 130 formed in center rail 94, and positioned proximate to a slider - disc contact interface proximate to the trailing edge of the slider. In the embodiment shown, trench 130 is transversely aligned and the length of the trench extends between opposed sides 132, 134 of center rail 94 and is opened at opposed sides to define a through channel between sides 132, 134. Trench 130 is illustrated in more detail in FIGS. 10-11.

As illustrated, trench 130 has a depth 136 and thickness 138. The depth 136 and thickness 138 are designed to reduce the capillary pressure of the meniscus relative to the disjoining pressure of the film to limit expansion of the meniscus area. In particular, depth 136 and thickness 138 are designed so that the separation distance between the capillary surface and the lubricant film layer ( $d_{120} + d_{136}$  - i.e. disc head - separation 120 + depth 136 of trench) is equal to or greater than  $2R_e$  (i.e.  $d_{120} + d_{136} \geq 2R_e$ ) to limit expansion of the meniscus beyond trench 130 and reduce capillary pressure to lower the meniscus force.

Preferably, the trench 130 is recessed a distance 140 from the transducer 98 of the slider 72. Distance 140 is relatively small to position the trench 130 close to the slider - disc interface to minimize stiction. Preferably, in an example embodiment, trenches 130 may have a depth 136 of  $0.3 \mu\text{m}$  and a thickness 138 of  $20 \mu\text{m}$ . The spaced distance 140 may be  $10 \mu\text{m}$  from the transducer. The trench 130 may be formed by known manufacturing processes, such as known photolithography techniques. Although a square bottom surface 141 is shown, it should be understood, that the invention is not limited to the exact configuration

shown and that the trench may have a rounded or "V" shaped (not shown) bottom surface 141.

FIG. 12 illustrates an alternate slider embodiment including trenches 130a-c located on center rail 94, and side rails 90, 92, respectively. In particular side rails 90, 92 include first and second ends 142, 144. First end is aligned relative to the leading edge of the slider and the second end 144 is spaced a distance 146 from the trailing edge of the slider. Trenches 130b-c are located proximate to the second end 144 of rails 90, 92, respectively to limit meniscus effect proximate to the side rails 90, 92 toward the trailing edge of the slider 72. Trenches 130 a-c are similarly dimensioned as trench 130 illustrated in FIGS. 9-11. Trenches 130b-c are preferably located 5  $\mu\text{m}$  from the second end 144 of rails 90, 92 and have a depth 136 of 0.3  $\mu\text{m}$  and a thickness 138 of 20  $\mu\text{m}$ .

FIGS. 13-16 illustrate alternate trench patterns for slowing meniscus growth by reducing the capillary pressure along the slider surface relative to the disjoining pressure of the lubricant film. FIG. 13 illustrates trench pattern 150 for slider 72. Trench pattern 150 includes a plurality of spaced transversely aligned elongated trenches 152, 154 (similar to trench 130) forming sequential rows of the trenches to form a line trench pattern. Although the trench pattern 150 is illustrated for center rail 94, trench pattern 150 may be included on side rails 90, 92 as described in relation to FIG. 12. Multiple transversely aligned, spaced trenches 152, 154 are included to collectively limit meniscus effect. In particular, the second trench 154 will slow the meniscus if the meniscus bridges the first trench 152. Although two trenches 152, 154 are

shown, it should be understood that any number of trenches may be included.

FIG. 14 illustrates another trench pattern 160. Trench pattern 160 includes a plurality of spaced  
5 longitudinally aligned trenches 162, 164. Longitudinally aligned trenches 162, 164 are spaced a distance 166 from the transducer elements and are located between sides 132, 134. Preferably, the trenches are recessed 20 microns from the sensor. In  
10 the embodiment shown, trenches 162, 164 are opened at ends 168, 169 at a leading edge of the center rail 94.

Although a specific embodiment of longitudinal trenches 162, 164, is shown, the invention is not limited to the specific number, orientation, etc shown.  
15 The multiple longitudinal trenches 162, 164 provide multiple voids at the contact interface to slow meniscus growth. Although the trench pattern 160 is illustrated for center rail 94, trench pattern 160 may be included on side rails 90, 92 as described in relation to FIG.  
20 12.

FIG. 15 illustrates alternate trench pattern 170 including a plurality of spaced transverse trenches 172, 174, 176 and a longitudinal trench 178 to form a combination trench pattern. Spaced transverse trenches  
25 172, 174, 176 are similar to trenches 152, 154 illustrated in FIG. 13. In the embodiment shown, longitudinal trench 178 extends from transverse trench 172 through trenches 174, 176 to an end 179 of the center rail spaced from the trailing edge and transducer  
30 98. Preferably, as shown, transverse trenches 172, 174, 176 extend between opposed sides 132, 134 of center rail 94 and longitudinal trench 178 is generally centered relative to sides 132, 134. Although a particular number, orientation and arrangement of transverse and

longitudinal trenches is shown, it should be understood that the invention is not limited to the specific embodiment shown, and is not limited to center rail 94.

FIG. 16 illustrates alternate trench pattern 180 including a plurality of alternately sloped trenches 182, 184 and 186, 188, which are sloped relative to the longitudinal and transverse axis of the slider. Sloped trenches 182, 186 and 184 and 188 intersect to form a cross pattern. Transverse trenches 190, 192 are included at the ends of the sloped trenches 182, 184, 186 and 188. Transverse trenches 190, 192 extend between sides 132, 134 of center rail 94. Sloped trenches 182, 184, 186 and 188 are opened to transverse trenches 190, 192. Although a particular embodiment of sloped trenches is shown, it should be understood that the invention is not limited to the specific embodiment shown and is not limited to the center rail 94.

The present invention is not limited to non-contacting recording and may be used for pseudo-contact recording as illustrated in FIG. 17 where the slider may intermittently contact the disc surface during operation. FIG. 17 illustrates an embodiment of a slider 200 for pseudo-contact recording. Like numbers are used to identify like parts to slider 72. As shown, the slider 200 is formed of a rigid member and includes shortened side rails 90-1, 92-1 and center rail 94. Ends of shortened side rails 90-1, 92-1 are spaced from the trailing edge 82. Side rails 90-1, 90-2 support pads 100a proximate to the leading edge and thus the trailing edge may intermittently contact the disc surface during operation. To reduce stiction, a trench pattern 130, 150, 160, 170 or 180 (only trench 130 shown) may be formed in center rail 94 proximate to the contact interface to limit growth of meniscus.

Although the present invention has been described with reference to preferred embodiments, workers skilled in the art will recognize that changes may be made in form and detail without departing from the spirit and scope of the invention. In particular, 5 although specific trench patterns are disclosed, the invention is not limited to the specific patterns disclosed.